

UpSac_50

c 1 2 3 4 5 6 7 8 9 10
c Primary HEC-50 data set. The data contained within this file and associated
c subordinate data files provide all supplemental input for the temperature /
c water quality component of HEC-50.

c. Extensive comments are included within the data set to provide insights
c. into the data preparation process. The definition and significance of the
c. individual data entries are provided in the Users Manual. Specific data
c. entries are defined in Exhibit 3 of the Users Manual.

c. The USBR-TMS interface utilizes comments identified by
c. "CV" - vertically segmented reservoir
c. "CL" - Longitudinally segmented reservoirs
c. "CS" - streams

Ti Thermal analysis, Upper Central Valley System
Ti Trinity, Lewiston, Whiskeytown, Shasta and Keswick Reservoirs
Ti Cottonwood Creek / record or CALSIM II

c. Flow at 24 hour time steps and water quality at 6-hour time steps.

JA 19910913 19920330 6 C 2 0

c. Two output files are specified. The "US_50.out" file is the traditional
c. printer output file. "US" is the GUI interface file which allow
c. interactive viewing of model results and ambient data. The complete GUI
c. file name is created by the model and takes the form of "iiii_nn.yy where
c. "iiii" is the user input (up to 5 characters), nn is the next available
c. sequence number and yy is the beginning year of simulation. A complete file
c. name of "US_03.91" would be the GUI output for the third run beginning in 1991.

JF out= UPSac_5q.out

c. GUI output interval for 6-hour time steps (Hours 6 & 18 - max and min)

c
JF gui = US 2

JF swm= some.swm

JF icr= 16jun98.dat

TEMPERATURE OUTPUT F

c... EXCEL compatible output file (CDF: "," replaced by "-")

EXCEL OUT FCST. 2XL

c	CDEC temperature sta.	FCST. 2XL	Mile	HEC-50 elem.
c	Lewiston (WQ-fish)			11
c	Spring Cr. PH			17
c	Shasta Dam			19
c	Keswick	301.5		37
c	Bonneview	289.5		49
c	Balls Ferry	276.2		62
c	Jellys Ferry	266.7		72
c	Bend Bridge	257.7		81
c	DWR temperature sta.	FCST. 2XL	Mile	HEC-50 elem.
c	Keswick	301.5		37
c	Balls Ferry	276.2		62
c	Jellys Ferry	266.7		72
c	Bend Bridge	257.7		81

c. flag element Parameter Identification
EXCEL ELEM 11 1 10 Lewiston TW Temp-F
EXCEL ELEM 17 1 99 Spring Cr. PH Temp-F

UpSac_50

EXCEL ELEM		19	1	99	Shasta Temp-F
cp-rm	200	301.5	1	500	Keswick Temp-F
cp-rm	180	289.5	1	500	Bonnevi ew Temp-F
cp-rm	178	276.5	1	500	Balls Ferry Temp-F
cp-rm	170	266.5	1	500	Jellys Ferry Temp-F
cp-rm	170	257.5	1	500	Bend Bri dge Temp-F

LakeProFile ResFCST. 2xl

c... the following will save the temperature profile for a single date

c. LakeproDate 220 temp 30-Apr-2004 12:00
Shasta Lake

c... omitting the date as below will save the indicated date/time for each year of simulation

LakeproDate	340	temp 09-Apr-	12:00
		Tri ni ty Lake	
LakeproDate	340	temp 31-May-	12:00
		Tri ni ty Lake	
LakeproDate	340	temp 30-Jun-	12:00
		Tri ni ty Lake	
LakeproDate	340	temp 31-Jul -	12:00
		Tri ni ty Lake	
LakeproDate	340	temp 31-Aug-	12:00
		Tri ni ty Lake	
LakeproDate	340	temp 30-Sep-	12:00
		Tri ni ty Lake	
LakeproDate	340	temp 30-Oct-	12:00
		Tri ni ty Lake	
LakeproDate	340	temp 30-Nov-	12:00
		Tri ni ty Lake	
LakeproDate	240	temp 30-Apr-	12:00
		Whi skytown Lake	
LakeproDate	240	temp 31-May-	12:00
		Whi skytown Lake	
LakeproDate	240	temp 30-Jun-	12:00
		Whi skytown Lake	
LakeproDate	240	temp 22-Jul -	12:00
		Whi skytown Lake	
LakeproDate	240	temp 31-Jul -	12:00
		Whi skytown Lake	
LakeproDate	240	temp 31-Aug-	12:00
		Whi skytown Lake	
LakeproDate	240	temp 30-Sep-	12:00
		Whi skytown Lake	
LakeproDate	240	temp 30-Oct-	12:00
		Whi skytown Lake	
LakeproDate	240	temp 30-Nov-	12:00
		Whi skytown Lake	
LakeproDate	220	temp 30-Apr-	12:00
		Shasta Lake	
LakeproDate	220	temp 31-May-	12:00
		Shasta Lake	
LakeproDate	220	temp 30-Jun-	12:00
		Shasta Lake	
LakeproDate	220	temp 22-Jul -	12:00
		Shasta Lake	
LakeproDate	220	temp 31-Jul -	12:00
		Shasta Lake	
LakeproDate	220	temp 31-Aug-	12:00
		Shasta Lake	
LakeproDate	220	temp 30-Sep-	12:00
		Shasta Lake	
LakeproDate	220	temp 30-Oct-	12:00

UpSac_50

LakeproDate Shasta Lake 220 temp 30-Nov- 12:00
Shasta Lake

OrderLakeProFile

c. The GUI output variables are defined on the "JG" Records. If these records are omitted, the default output is limited to temperature, TDS, flow and water surface elevation. The "JG" Record references the parameter numbers of Table L9 in the documentation. Up to 3 parameters may be included with the appropriate scaling factors (i.e., F1-F3). Flows and elevations may be included. For temperature simulation, GUI output is limited to:

	ID1	F1	ID2	F2	ID3	F3	min	max	
JG	1	1.					40	80	Temperature, F
*F	*T								
JG	2	1.					990	1010	Inflow Tracer
JG	28	1.					0	40000	Flow, cfs
		*T							
JG	29	1.					600	1200	Elevation, Ft

ZW JAN05. dss A=UPPER_SAC_50 E=1DAY F=SIMULATION

c. USBR option: specify b part in the DSS file path name instead of default CP & RM

JZ	-340	239.5	TEMP	B=TRINITY
JZ	-330	230.5	TEMP	B=LEWISTON
JZ	-242	190.5	TEMP	B=CLEAR_CR_TUNNEL
JZ	-230	180.1	TEMP	FLOW B=WHISKEYTOWN
JZ	-212	304.5	TEMP	B=SPRG_CR_TUNNEL
JZ	-220	310.9	TEMP	B=SHASTA
JZ	-200	301.5	TEMP	FLOW B=KESWICK
JZ	-180	289.5	TEMP	FLOW B=CLEAR_CR
JZ	-180	10.0	TEMP	B=IGO
JZ	-180	0.5	TEMP	FLOW B=DS_CLEAR_CR
JZ	-178	284.0	TEMP	B=AI RPORT_RD
JZ	-178	280.5	TEMP	B=COW_CR
JZ	-178	276.2	TEMP	FLOW B=BALLS_FERRY
JZ	-170	266.5	TEMP	FLOW b=JELLYS_FERRY
JZ	-170	259.9	TEMP	FLOW B=BEND_BR
JZ	-160	243.1	TEMP	FLOW B=RED_BLUFF
JI	1		TEMP	B=SHASTA_INFLOW
JI	2		TEMP	B=TRINITY_INFLOW

c. Meteorological data may reside in a subordinate ASCII input file or in DSS. The subordinate input file contains all EZ and associated ET Records. The meteorological data interval should be compatible with the water quality time step. These data are normally placed in DSS file or in the subordinate file to streamline and reduce the size of the main data file. Note that when the end of a subordinate meteorological data file is reached, the file is rewound and the data are reused. This option is normally used if average meteorological data are being considered. The DSS input option requires data for

c. the entire simulation period.

c. An example of the meteorological data format is provided below.

c. [Note that the ES (saturated vapor pressure), W.TMP (Temperature of a 10-foot deep pool) & EVAP (accumulative evaporation) are for information purposes only]

c. EZ	YEAR	MMDDHH	ET	KT	RAD	WIND	ES	W. TMP	EVAP
			Temp	Coeff	Rad.	Speed	mb	F	ft
c. ET	1989	010106	25.64	75.90	0.0	9.87	6.69	31.91	0.00
c. ET	1989	010112	46.96	107.08	1735.2	12.18	7.04	31.90	0.00

UpSac_50

c. EZFILE= ShastaDM.met
c. EZEND

c. DSS input				
c. A Part	B Part	C Part	F Part	E Part D
Part				
c. MET DATA	GERBER2SHASTA	EQTEMP	AVERAGE	6HOUR
01JAN1990 - 01DEC1999				
c. - - - - -	- - - - -	EXRATE	AVERAGE	6HOUR
01JAN1990 - 01DEC1999				
c. - - - - -	- - - - -	SWRAD	AVERAGE	6HOUR
01JAN1990 - 01DEC1999				
c. - - - - -	- - - - -	WIND	AVERAGE	6HOUR
01JAN1990 - 01DEC1999				

c. Note that the "C" part may be omitted if these C part identifications are used
c. If the "C part" is included, the input sequence must be for ET, KE, solar rad and wind

c. the "ZR" triggers DSS input
c. EZ 1 1 6 6 ZR pr Gerber (CIMIS) / Shasta Dam (USWS)
EZ 1 6 ZR Gerber (CIMIS) / Shasta Dam (USWS) >> wind * 2
ET A=met data B=Gerber2Shasta E=6HOUR F=AVERAGE

EZEND

Shasta Dam TCD opp file TCD_opp.log
c. Shasta Dam TCD date 11Mar1999
c. Shasta Dam outlet opp shasta_outlet_flows.dat

list

c. The QC Records triggers simulation of water quality parameters in addition to temperature.

QC 1 1 0 0 0 0 0 0

TQ Inflow Tracer

L1 30 1

c. IRCP	METL	IPL	SDZ	EDMAX	XQPCT	XQDEP	IZ	FICEL
c. CV Clair Engle Lake (Trinity)								
CV Trinity River, Clair Engle Lake	, 240					1	0	0
L2 340	1	0	3.2814	-.8	.3			
c. FK2R	FK2C	FK2S	SFMET1	SFMET2	sfmet3			
L2 1	1	1	-2.	1.	1.05			
C. Scaling factors for====>		EQT1	EQT2	KEF				

C. SEASONAL EXCO								
LE	1	22	90	20	120	12	180	15
LE	240	15	366	22				

c	1	2	3	4	5	6	7	8	9	10
c										
LR	I	IN	F	2	1.	5000	Trinity	River		.035

L3 0 .12E-6 .12E-4 -.7 -15. .25
LB .001 5. 10.

L5	400	2400	2000
L6	100	12000	2365
c. L7	400	4600	2030
L7	400	11100	2110

UpSac_50

L8		200	400	500	600	700	800	880	960	1040
L8	1120	1200	1280	1360	1440	1520	1600	1620	1640	1660
L8	1680	1700	1720	1740	1760	1780	1800	1820	1840	1860
L8	1880	1900	1920	1940	1960	1980	2000	2020	2040	2060
L8	2080	2100	2120	2140	2160	2180				
c. RE	45	1950	1960	1970	1980	1990	2000	2010	2020	2030
c. RE	2040	2050	2060	2070	2080	2090	2100	2110	2120	2130
c. RE	2140	2150	2160	2170	2180	2190	2200	2210	2220	2230
c. RE	2240	2250	2260	2270	2280	2290	2300	2310	2320	2330
c. RE	2340	2350	2360	2370	2380	2390				
L9 temp	ICR		1							
L9 CONS1	1000									

- c. No coefficients are required for thermal analysis or for conservative parameters.
- c. Records containing values of coefficients and rate constants used in the equations for various water quality parameters would be inserted here. The coefficients specified on records KA through KE are global and pertain to all reservoirs and stream reaches. These coefficients can only be set with the first reservoirs data. If these data are not entered at that time, the default values would apply.
- c. The remaining records would contain coefficients and rate constants that apply to specific reservoirs. These coefficients must be provided for the first reservoir in the system since many coefficients have no default values. These coefficients would apply to all subsequent reservoirs and stream sections if not respecified with the subsequent reservoir and stream data sets.

EL

c.	IRCP	METL	IPL	SDZ	EDMAX	XQPCT	XQDEP			
c.	CL	Lewiston Lake								
CL	Lewiston Lake,	Trinity River,	Trinity River,	230.0,	208					
L2	320	1		8.0	.4	1				
c.	FK2R	FK2C	FK2S	SFMET1	SFMET2	sfmet3				
L2	1	1	1	1.	1.00	1.0				
C.	Scaling factors	for==>	EQT1	EQT2	KEF					

LS 5.0 1000

C. Layering

lt	9	.01E-4	1.E-4	2.E-6	-2.	1.10				
lu		.11	.11	.11	.11	.11	.11	.11	.11	.12
R2	1	1000	1880	100	1890	300	1900	450	1910	550
R3	1920	600								
LI		CP	330	1.	Trinity River					
LV	US	.11	.11	.11	.11	.11	.11	.11	.11	.12
R2	2	1000	1875	100	1880	200	1890	350	1900	500
R3	1910	600	1920	700						
LV	US	.11	.11	.11	.11	.11	.11	.11	.11	.12
R2	3	1000	1870	100	1880	200	1890	400	1900	600
R3	1910	800	1920	900						
R2	4	1000	1865	100	1880	200	1890	300	1900	450
R3	1910	600	1920	700						

UpSac_50

LV	DS	-1	8	1.33						
R2	5	1000	1860	100	1870	150	1880	300	1890	400
R3	1900	550	1910	700	1920	800				
R2	6	1000	1855	100	1870	200	1880	300	1890	450
R3	1900	550	1910	600	1920	660				
R2	7	1000	1850	100	1865	250	1880	500	1890	650
R3	1900	800	1910	900	1920	960				
R2	8	1000	1845	100	1860	200	1880	250	1900	300
R3	1920	350								
R2	9	1000	1840	100	1860	180	1880	280	1900	350
R3	1920	400								

LW DS 1 1860. 100. 0

L9 TEMP 10. 0
L9 CONS1 1000

EL

c ***** Dummy Reservoir: Clear Creek Tunnel inflow to Whiskeytown *****

c. ID	IRCP	METL	IPL	SDZ	EDMAX	XQPCT	XQDEP	IZ	FICEL
L2	244	1			3.	.4	1		
LA		12.							
RS	5	2.	12.	24.	36.	52.			
RA	5	2.	3.	5.	6.	7.			
RE	5	1200	1205	1210	1212	1214			

LS 1.0 200 0 12 3 1105

R1	1	10	2	40	100	0			
LI	R		5	1.	Clear Creek Tunnel				
R1	2	10	2	40	100	0			

L9 TEMP 10. 0
L9 CONS1 1000

EL

c. IRCP	METL	IPL	SDZ	EDMAX	XQPCT	XQDEP
c. CV Whiskeytown Lake						
CV Clear Creek, Whiskeytown Lake,			21.0,	16.6		
L2 240	1	0	3.2814	-.8	.25	1
c. FK2R	FK2C	FK2S	SFMET1	SFMET2	sfmet3	
L2 1	1	1	-1.	1.	1.10	
C. Scaling factors for====>			EQT1	EQT2	KE	

C. SEASONAL EXCO									
LE	1	9	120	9	180	6	300	6	
LE	366	9							

c	1	2	3	4	5	6	7	8	9	10
c										
LR	I	IN	F	3	1.	5000	Clear / Whiskey	Creek		.020
c. Temperature Curtain - no entrainment										
LR	cp		242	1.	5000	Clear Creek	PH			.020

L3	0	.5E-6	.2E-4	-.7	-15.	.25
LB	.001	5.	10.			

UpSac_50

L5 80 900 970
 L6 80 15000 1200
 LD 480 1080

I 8 100 150 200 250 300 350 400 450 500
 L8 550 600 800 1000 1100 1200 1300 1400 1500 1600
 L8 1700 1800 1900 2000 2100 2200 2300 2400

c. RE 26 980 990 1000 1010 1020 1030 1040 1050 1060
 c. RE 1070 1080 1090 1100 1110 1120 1130 1140 1150 1160
 c. RE 1170 1180 1190 1200 1210 1220 1225

L9 temp ICR 2
 L9 CONS1 1000

EL

c ***** Dummy Reservoir: Spring Creek Tunnel inflow to Keswick *****
 c. ID IRCP METL IPL SDZ EDMAX XQPCT XQDEP IZ FICEL
 L2 214 1 3. 4 1
 LA 12.
 RS 5 2. 12. 24. 36. 52.
 RA 5 2. 3. 5. 6. 7.
 RE 5 580 585 590 592 594

LS 1.0 200 0 12 3 1105
 R1 1 10 2 40 100 0
 LI R 6 1. Spring Creek Tunnel
 R1 2 10 2 40 100 0

L9 TEMP 10. 0
 L9 CONS1 1000

EL

c. IRCP METL IPL SDZ EDMAX XQPCT XQDEP
 c. CV Lake Shasta
 CV Sacramento River, Lake Shasta, 313, 311
 L2 220 1 1 3. 2814 -. 8 . 3 1
 c. FK2R FK2C FK2S SFMET1 SFMET2 sfmet3
 L2 1 1 1 -. 1 .97 1. 1
 C. Scaling factors for====> EQT1 EQT2 KE

C. SEASONAL EXCO
 LE 1 14 120 14 150 10 300 10
 LE 366 14

c 1 2 3 4 5 6 7 8 9 10
 c | | | | | | | | | |
 LR I N F 1 1. 15000 flow weighted average . 0175

L3-. 1e-6 1. E-6 . 225E-4 -. 7 -10. . 33
 LB . 001 5. 10.

L5 603 22000 942 603 24500 842 680 17500 742 -1
 L6 300 150000 1060
 L7 1000 18000 817

L8 28 34 47 59 68 85 104 123 145
 L8 174 232 238 276 316 366 467 459 502 557
 L8 678 683 749 819 890 969 1044 1182 1205 1289
 L8 1376 1468 1554 1657 1752 1854 1951 2060 2175 2294
 L8 2388 2408 2543 2656 2770 2895 2974 3023 3108 3133

UpSac_50

c. Temperature objectives penalty function and temperature targets

PL	1	2.	100	0	-2	0	0	0	
c. PT		1.	16.0	128.	10.8	150.	10.0	151.	11.0
c. PT		161.	10.8	170.	10.6	176.	9.5	197.	8.1
c. PT		232.	8.7	268.	11.2	288.	12.2	366.	20.0
c. PT		1.	16.0	197.	8.1	210.	8.6	212.	8.8
c. PT		215.	8.7	225.	8.5	226.	9.2	240.	9.5
c. PT		255.	10.1	273	11.2	288.	12.4	366.	20.0
c. PT		1.	16.0	197.	8.1	210.	8.6	212.	8.8
c. PT		215.	8.5	225.	8.3	226.	9.0	240.	9.3
c. PT		255.	9.9	273	11.2	288.	12.4	366.	20.0
c. PT		1.	16.0	124.	16.0	130.	10.0	138.	9.5
c. PT		150.	9.5	155.	11.6	161.	9.7	175.	9.7
c. PT		176.	8.9	197.	7.5	232.	8.5	366.	20.0
c. PT		1.	16.0	114.	16.0	115.	13.3	122.	11.5
c. PT		123.	11.8	158.	11.5	161.	12.0	175.	12.9
c. PT		176.	11.1	197.	10.0	232.	10.2	366.	20.0
c. PT		1.	16.0	124.	16.0	130.	10.0	138.	9.5
c. PT		150.	9.5	155.	11.6	161.	9.7	175.	9.7
c. PT		176.	8.9	192.	7.0	232.	8.0	366.	20.0
c. PT		1.	16.0	120.	16.0	121.	11.6	130.	11.6
c. PT		131.	10.3	155.	10.9	161.	10.2	175.	10.2
c. PT		176.	9.4	212.	7.1	242.	8.2	366.	21.0
c. PT		1.	16.0	120.	16.0	121.	11.7	130.	11.4
c. PT		131.	10.5	161.	10.5	175.	10.4	176	9.4
c. PT		212.	7.1	242.	8.2	273	12.0	366.	16.0

L9 temp ICR 3
L9 CONS1 1000

EL

*****			Dummy	Reservoir	below	Lewiston	Dam *****		
c. ID	IRCP	METL	IPL	SDZ	EDMAX	XQPCT	XQDEP	IZ	FICEL
L2	300	1			3.	.4	1		
LA		12.							
RS	5	2.	12.	24.	36.	52.			
RA	5	2.	3.	5.	6.	7.			
RE	5	580	585	590	592	594			
LS			1.0	200	0	12	3	1105	
R1	1	10	2	40	100	0			
LI		CP	300	1.	Tri ni ty	Ri ver			
R1	2	10	2	40	100	0			
L9 TEMP		10.							
L9 CONS1		1000							

EL

*****			Dummy	Reservoir	below	Whiskeytown	Dam *****		
c. ID	IRCP	METL	IPL	SDZ	EDMAX	XQPCT	XQDEP	IZ	FICEL
L2	230	1			3.	.4	1		
c. FK2R		FK2C	FK2S	SFMET1	SFMET2	sfmet3			
L2	1	1	1	-.1	1.	1.1			

C. Scaling factors for====>				EQT1	UpSac_50 EQT2	KE			
LA		12.							
RS	5	2.	12.	24.	36.	52.			
RA	5	2.	3.	5.	6.	7.			
RE	5	580	585	590	592	594			
LS			1.0	200	0	12	3	1105	
R1	1	10	2	40	100	0			
LI		CP	230	1.	Spring Creek				
R1	2	10	2	40	100	0			
L9 TEMP		10.	0						
L9 CONS1		1000							

EL

c. IRCP	METL	IPL	SDZ	EDMAX	XQPCT	XQDEP			
c. CL Keswick Lake to Spring Creek						310			
CL Keswick Lake, to Spring Creek, Sacramento River,						310, 302.7			
L2	200	1		8.0	.4	1			
c. FK2R	FK2C	FK2S	SFMET1	SFMET2	sfmet3				
L2	1	1	1	-.1	1.	1.1			
C. Scaling factors for====>			EQT1	EQT2	KE				

LS		5.0	1000						
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C. Layering

lit	5	.01E-4	1.E-4	1.E-6	-5.	1.33				
lu		.20	.20	.20	.20	.20				
R2	1	3900	574.0	220.0	577.8	264.4	581.5	308.8	585.3	353.1
R3	589.0	397.5	592.8	441.9						
LI		CP	210	1.	Sacramento below Shasta					
R2	2	3900	567.3	220.0	572.7	274.3	578.2	328.6	583.6	382.9
R3	589.0	437.3	594.4	491.6						
R2	3	3900	560.6	220.0	567.7	284.3	574.8	348.5	581.9	412.8
R3	589.0	477.0	596.1	541.3						
R2	4	3900	553.9	220.0	562.7	304.1	571.5	388.3	580.2	472.4
R3	589.0	556.5	597.8	640.6						
R2	5	3900	547.2	220.0	557.7	324.0	568.1	428.0	578.6	532.0
R3	589.0	636.0	599.5	740.0						
R2	6	3900	540.5	220.0	552.6	343.9	564.8	467.8	576.9	591.6
R3	589.0	715.5	601.1	839.4						
R2	7	3900	533.8	220.0	547.6	363.8	561.4	507.5	575.2	651.3
R3	589.0	795.0	602.8	938.8						
R2	8	3900	527.1	220.0	542.6	383.6	558.1	547.3	573.5	710.9
R3	589.0	874.5	604.5	1038.1						
R2	-12	3900	520.4	220.0	537.6	403.5	554.7	587.0	571.9	770.5
R3	589.0	954.0	606.2	1137.5						

c. CL Keswick Lake, Spring Creek branch						304.4			
CL Keswick Lake, Spring Creek branch, Spring Creek Tunnel,						304.0, 301.402			

UpSac_50

R2	10	1000	550.0	100.0	559.8	174.4	569.5	248.8	579.3	323.1
R3	589.0	397.5	598.8	471.9						

LI CP 212 1. Spring Creek Tunnel

R2	-12	1000	522.0	200.0	538.8	309.0	555.5	418.0	572.3	527.0
R3	589.0	636.0	605.8	745.0						

c. CL Keswick Lake below Spring Creek 304
 CL Keswick Lake, below Spring Creek, Sacramento River, 302.7, 302

R2	12	3500	513.7	220.0	532.5	483.0	551.4	746.0	570.2	1009.0
R3	589.0	1272.0	607.8	1535.0						

R2	13	3500	507.0	220.0	527.5	443.3	548.0	666.5	568.5	889.8
R3	589.0	1113.0	609.5	1336.3						

L9 TEMP 8. 0
 L9 CONS1 1000

EL

c ***** Dummy Reservoir - Cottonwood Creek gauge *****

c. ID	IRCP	METL	IPL	SDZ	EDMAX	XQPCT	XQDEP	IZ	FICEL
L2	176	1			3.	.4	1		
LA		12.							
RS	5	2.	12.	24.	36.	52.			
RA	5	2.	3.	5.	6.	7.			
RE	5	580	585	590	592	594			
LS			1.0	200	0	12	3	1105	
R1	1	10	2	40	100	0			
LI	I N F		12	1.	Cottonwood Creek				
R1	2	10	2	40	100	0			

L9 TEMP 15. 0
 L9 CONS1 1000

EL

c. -1 <=== TO PRINT AFTER EACH REACH
 c. 1 <=== to print stream geometry data
 S1 30 1 0

c. The input sequence for the S2 Records controls the phasing of the reservoir simulation. The input sequence must progress from upstream to downstream.
 c. If the upstream control point (S2.1) corresponds to a reservoir number (L2.1), then the reach is an upstream limit of a stream section. If the downstream control point (S2.3) corresponds to control point named as an inflow to a reservoir (LI.2 = "CP"), then the reach is the downstream limit of the stream section.

CS Trinity River, below Trinity Dam
 S2 340 240. 330 230.0 1.0

c. A dummy reservoir is needed below Lewiston and Whiskeytown so that these reservoirs will be simulated prior to the diversion to Whiskeytown and Keswick.

c. Each reservoir must be separated by a stream reach. The -0.1 indicates that the reach serves as a conveyance reach in which no changes in temperature are to be computed. (Cross section data are not required.)

S2 320 220.2 300 220.0 -0.1

UpSac_50

CS Clear Creek Tunnel
 S2 244 210.0 242 209.8 -0.1

c. Clear Creek, below Whiskeytown Dam
 S2 240 180.2 230 180.0 -0.1

CS Spring Creek Tunnel
 S2 214 314.0 212 313.8 -0.1

CS Sacramento River, below Shasta Dam
 S2 220 311. 210 309.5 0.75

CS Clear Creek, below Whiskeytown Dam
 S2 230 16.5 180 0.0 1.03

CS Sacramento River, Keswick Dam to Clear Creek
 S2 200 302.0 180 289.0 1.0

SI QD W 298.5 -1 1. ACID Canal
 SI I I N F 292.5 11 1.0 all creeks

CS Sacramento River, Clear Creek to Cow Creek
 S2 180 289. 178 280.0 1.0

SI I I N F 284.5 11 .15 Churn Creek
 SI I I N F 280.1 11 .85 Cow Creek

CS Sacramento River, Cow Creek to Cottonwood Creek
 S2 178 280.0 174 273.0 1.0
 SI I I N F 277.3 11 .80 Bear+Ash Creek
 SI I I N F 273.5 11 .20 Anderson Creek

c. Cottonwood Creek to Sacramento River
 S2 176 6.0 174 0.0 1.0

CS Sacramento River, Cow Creek to Bend Bridge
 S2 174 273.0 170 260.0 1.0
 SI I I N F 271.3 10 1.0 Battle Creek

CS Sacramento River, Bend Bridge to Red Bluff Diversion Dam
 S2 170 260. 160 243.0 1.0

SI I I N F 253.3 10 .5 Paynes Creek
 SI I I N F 244.3 9 .5 Red Bank + Reeds Creek

c.	US CP	DS CP	METZ DC	unused BEDDC	K20PP BEDDEP	RK2MI IZ	RK2 I CEDEP	K2mi n HEX1	K2max HEX2	HEX3
SR	340	330	1	.010	2	0	0	1.0	5.0	
SR	244	212	0.44	.010	0.5	0	0	1.0	1.0	1.0
SR	220	210	0.44	.010	0.5	0	0	-1.0	1.	0.9
SR	230	180	0.44	.010	0.5	0	0	1.0	5.0	0.9
SR	200	180	0.44	.010	0.5	0	0	1.0	5.0	1.0
SR	180	160	0.44	.010	0.5	0	0	-1.0	.8	0.9
SR			0.44	.010	0.5	0	0	-0.5	.9	0.9

c. nolist

UpSac_50

c. Alternative or subordinate files may be used to input the cross-section data to streamline and reduce the size of the main data file. A partial listing of the "Xsec_s3.dat" file follows. The S3 Records define the cross-section geometry and flow characteristics. These data include the relationship between elevation, cross-section area, top width and flow. As a minimum, cross-section data must be supplied at each control point, but should be input in sufficient detail as to represent the hydraulic characteristics of the stream reach. The flow table must also cover the expected range of flows.

c.	CP	Mile	Elev	Area	Width	Flow	Vel
c. S3	340	150.0	1948.00	202.8	86.6	.001	.00
c. S3			1948.70	264.2	88.8	179.0	1.43
c. S3			1949.40	326.7	90.1	394.0	1.82
c. S3			1950.10	390.1	90.9	560.0	2.20
c. S3			1950.70	444.8	91.3	869.0	2.63
c. S3			1951.20	490.6	91.8	1200.0	3.06
c. S3			1951.70	536.6	92.4	1827.0	3.41
c. S3			1952.30	592.7	94.0	2267.0	3.83
c. S3			1952.90	650.3	97.7	2746.0	4.22
c. S3			1954.40	814.4	119.9	3938.0	4.84
c. S3			1955.60	964.0	129.2	5475.0	5.68
c. S3			1957.00	1155.4	145.0	7395.0	6.40
c. S3			1958.30	1353.8	159.9	9730.0	7.19
c. S3			1959.50	1551.2	168.9	12515.0	8.07
c. S3			1960.70	1758.2	176.2	15784.0	8.98
c. S3			1961.80	1952.8	177.6	19567.0	10.02
c. S3			1962.90	2148.5	178.2	23894.0	11.12
c. S3			1964.10	2362.9	179.1	28797.0	12.19
c. S3			1965.30	2578.3	179.9	34304.0	13.31
c. S3			1966.50	2794.5	180.7	40444.0	14.47

c. Actual Stream cross-section data
 S3FILE= S3_FCST.dat
 S3END

ES

nolist

C... TRIBUTARY INFLOW DATA
 I1 P 20000401 20151231

c. One or more alternative input files are allowed for input of tributary inflow data. All inflow data for this application are input via file "Tri b_Q.dat" as specified by the "ETFILE=" Record. The file contains comments regarding the data for the first tributary.

I2FILE= Tri b_Q.dat
 I2END

EI

C. Gate operation data determine operation of the outlets.
 c. Withdrawal sequence is Power, Flood control (low Level outlets) spillway.

c. yyyymmdd
 G1 20000401 20201231
 G2 340 20000401 2400 12000 11100 0 312

					UpSac_50				logoff	
C										
G2	320	20000401	900	1500	0	0				12
G2	244	20000401	900	1500	0	0				12
G2	214	20000401	900	1500	0	0				12
G2	230	20000401	900	1500	0	0				12
G2	240	20000401	900	1500	0	0				12
G2	200	20000401	900	1500	0	0				12
G2	300	20000401	900	1500	0	0				12
c. G2	220	20000401	64000	150000	18000		2	18000	2	312
c. Seasonal!!	G2	220	19210101	10.77						
G2	220	20000401	20.00							
G2	220	20150203	20.00							
G2	220	20150501	13.00							
G2	220	20150515	11.38							
G2	220	20150529	11.38							
G2	220	20150601	11.90							
G2	220	20150630	11.90							
G2	220	20150701	10.50							
G2	220	20150802	10.50							
G2	220	20150905	10.50							
G2	220	20150910	11.38							
G2	220	20151001	11.38							
G2	220	20151101	13.00							
c									logoff	
ER										