

Sediment Transport Analysis and Creek Restoration- Field Experiences

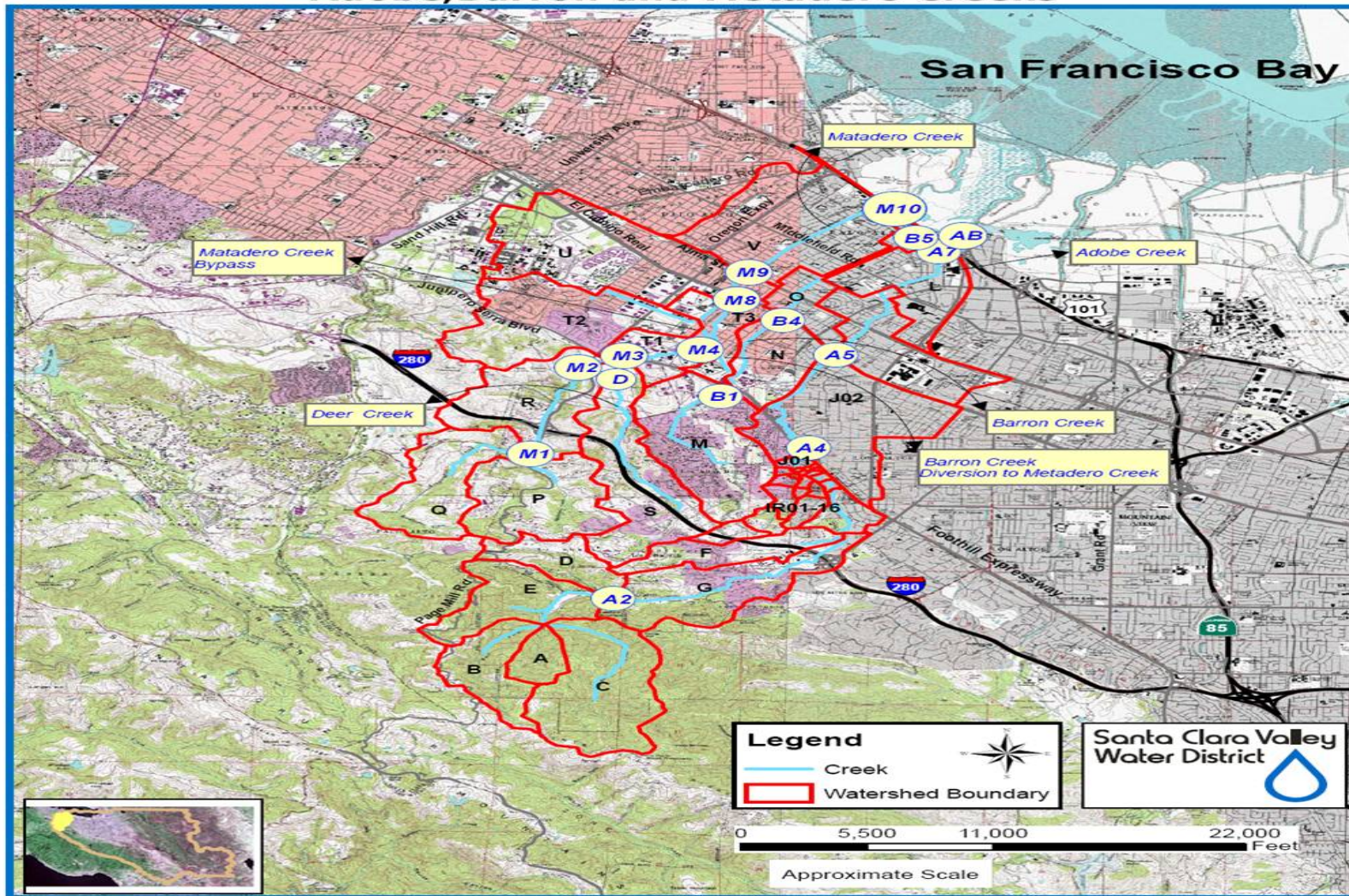
**4th Hydromodification Seminar & Workshop –
Sediment Management and Modeling
November, 21, 2013**

Topics

- Santa Clara County HMP program
- Stable channel design
- SCVWD regional bankfull curves
- Channel stability analysis

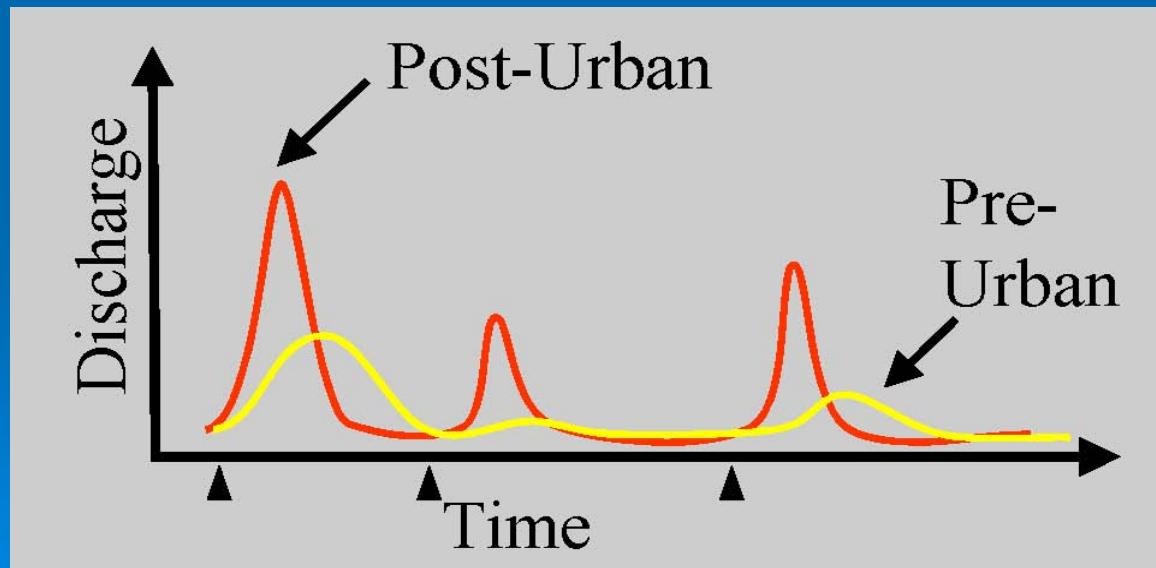
Urbanized Watersheds

Watershed Boundary Adobe, Barron and Metadero Creeks



Effects of hydrology by Urbanization

- Less infiltration / evapotranspiration
- More surface runoff (increased volume)
- Runoff leaves the site faster (increased peak flows)
- Runoff occurs more often (increased frequency)
- More runoff conveyed directly to creek



Thompson Creek Undermining outfall structure





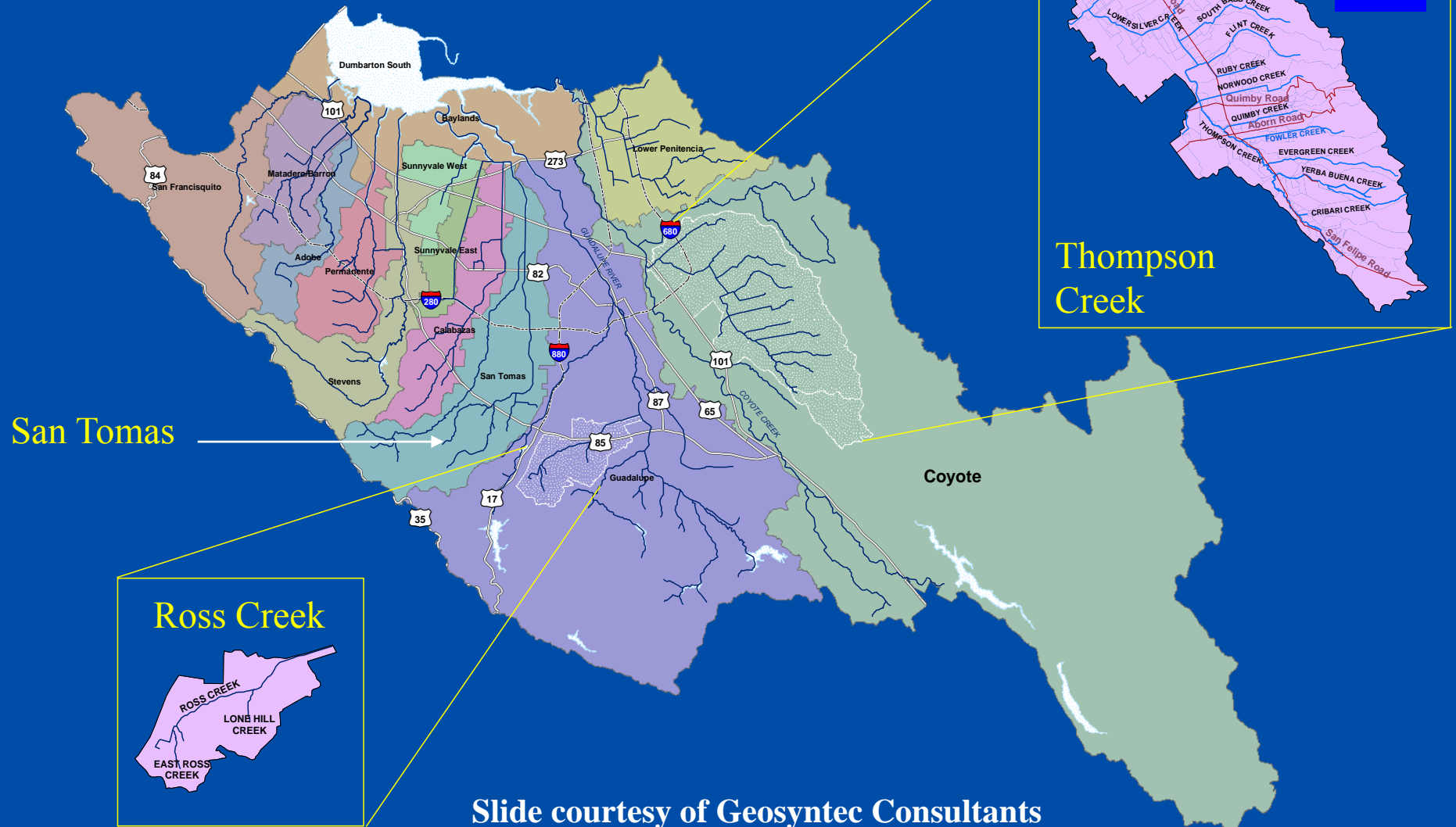
Incising channel bed on Yerba Buena Creek



Unurbanized Stable Stream

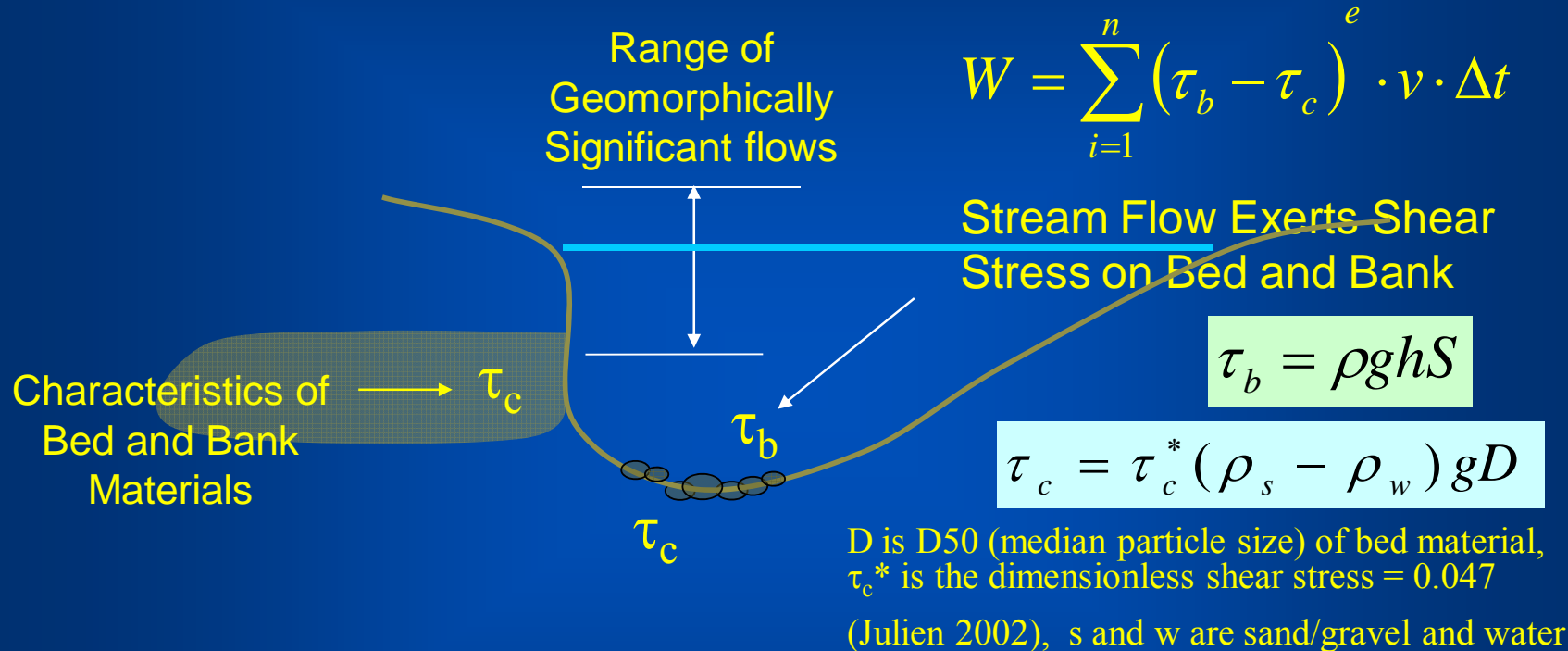


Subwatersheds Assessed under HMP



Slide courtesy of Geosyntec Consultants

Velocity, Shear Stress and Excess Total Work (W) based on Flow-Duration Histogram

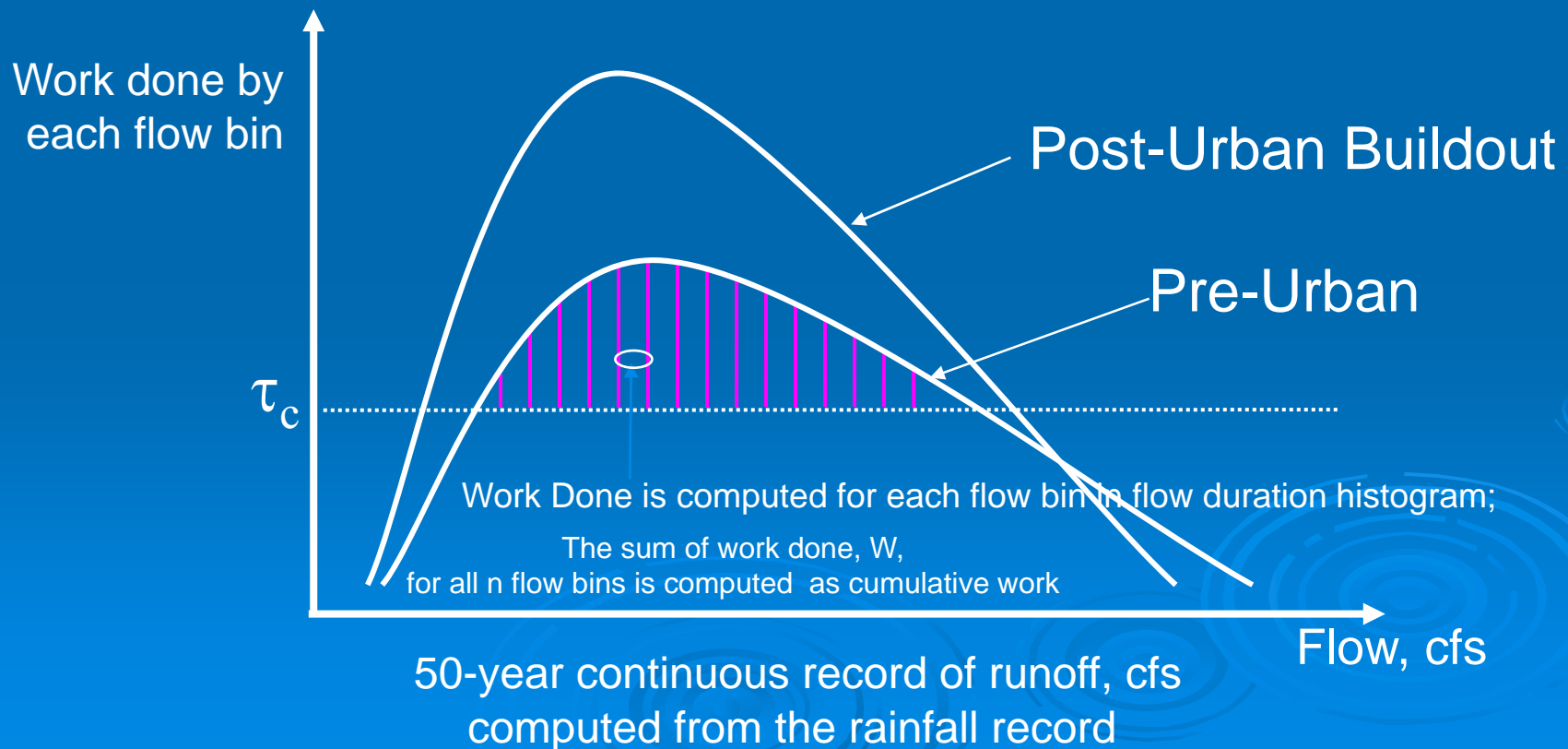


τ_c Critical Shear Stress of bed or weakest layer of bank at cross-section
Lower of the two values applies; if weak layer not at bottom $\tau_c = \tau_{c\text{bank}} + \rho g S h_{\text{bank}}$

v Mid-stream velocity observed over a duration Δt Which is a time period in histogram
n = number of separate flow bins in the flow duration histogram, e = 1 for computations shown

Increase Critical Shear Stress to Reduce Erosive Work Done (W_i)

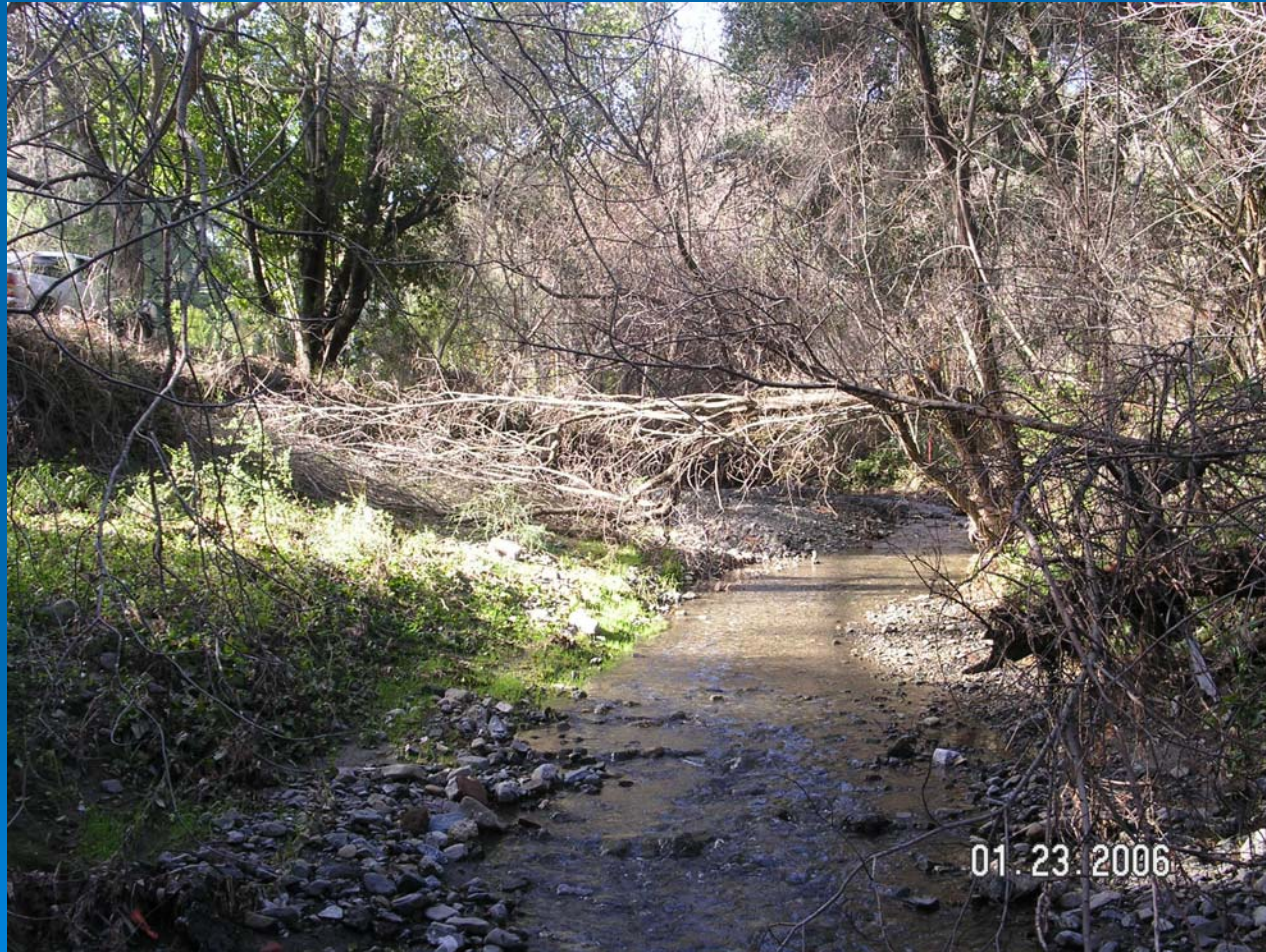
$$W_i = [(\tau_b - \tau_c)^{1.5} \cdot v \cdot \Delta t]_i \quad EP = W_{\text{existing}} / W_{\text{pre-urban}}$$



Stable Channel Design Procedure

1. Determine bankfull cross-sectional geometry
2. Develop equilibrium slope via. sediment transport modeling (SAM or HEC-6)
3. Identify hardpoints in project reach
4. Layout cross-section and profile and, if necessary, locations of grade control structures
5. Design surface protection

Remnant of Pre-urbanization channel geometry



Bankfull Channel Measurement

Note how bankfull channel is formed within stable flood conveyance channel

BF = bankfull

BF bench or
BF floodplain
width

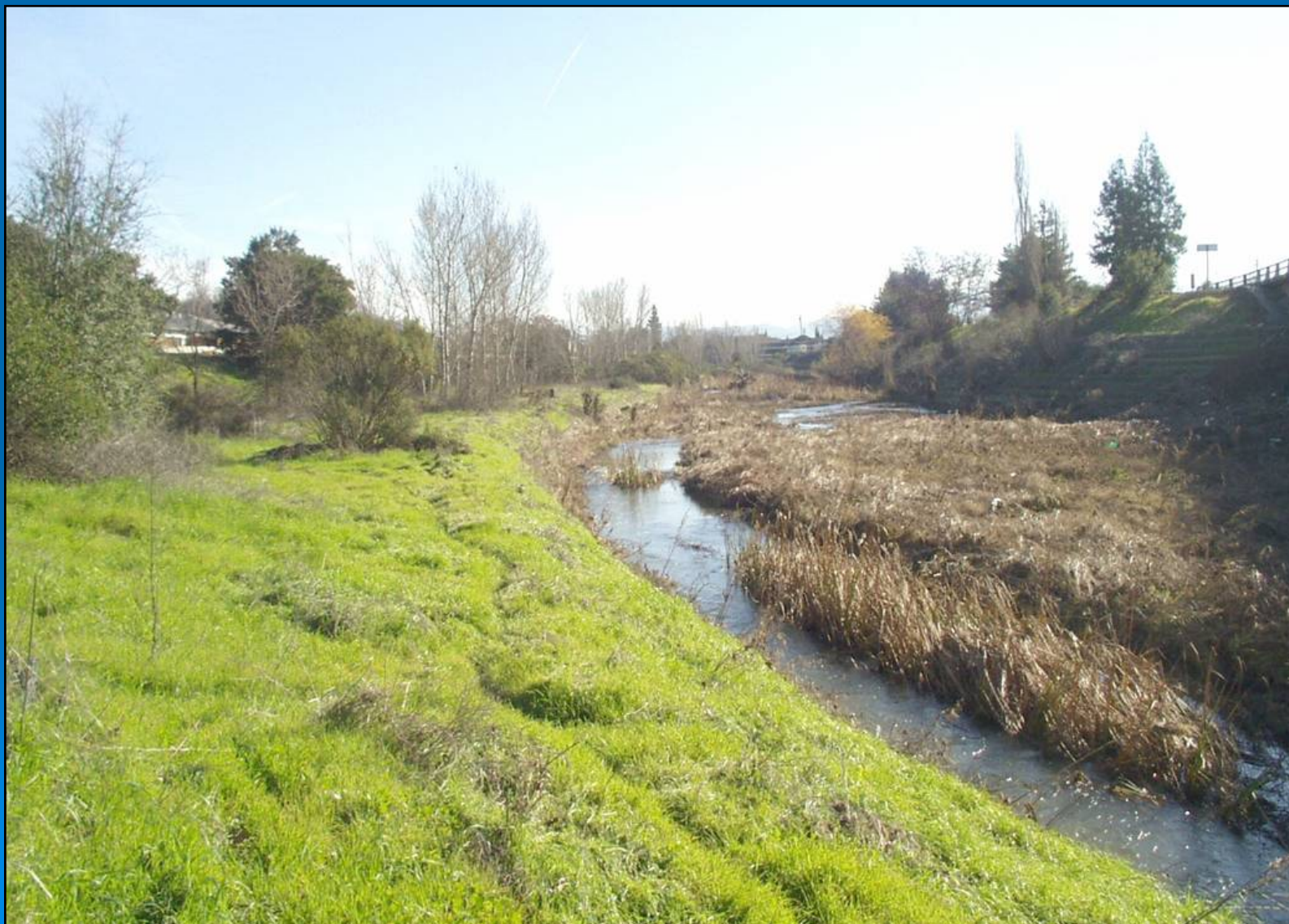
TH = Thalweg



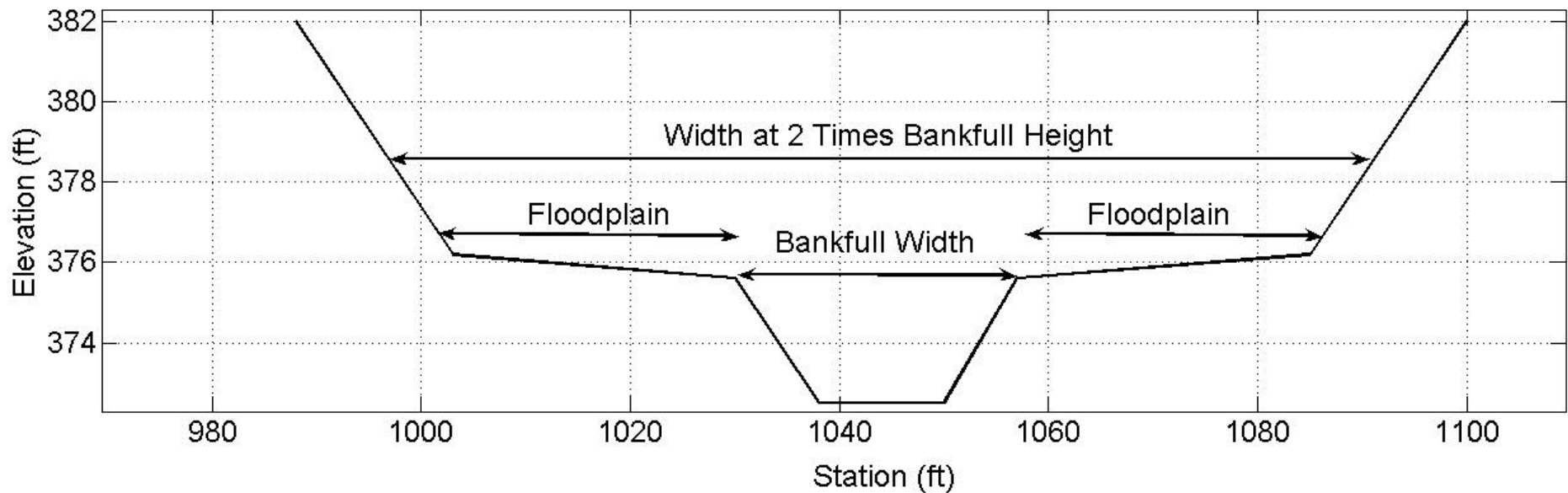
**2H:1V bank slope
for bankfull channel**

2H:1V bank slope

Guadalupe River at Almaden Expressway



Bankfull and Floodplain

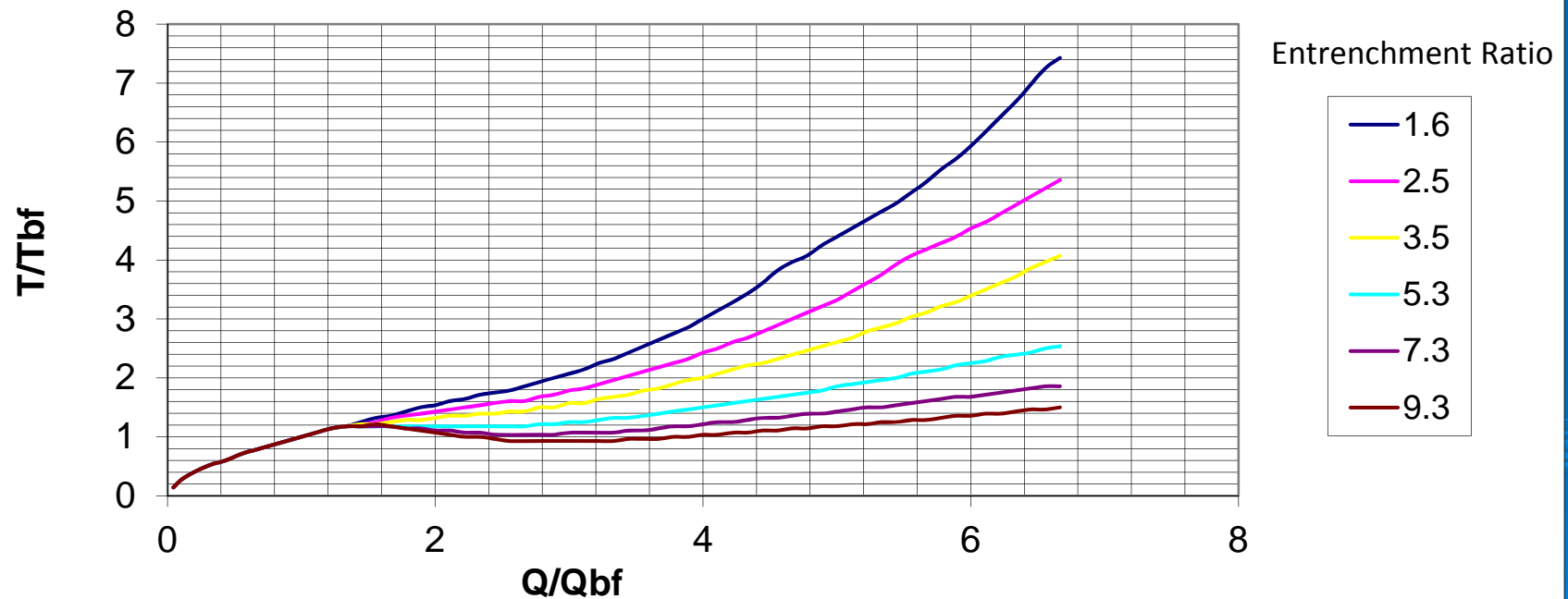


Entrenchment Ratio = ratio of channel width at 2x bankfull depth to bankfull depth

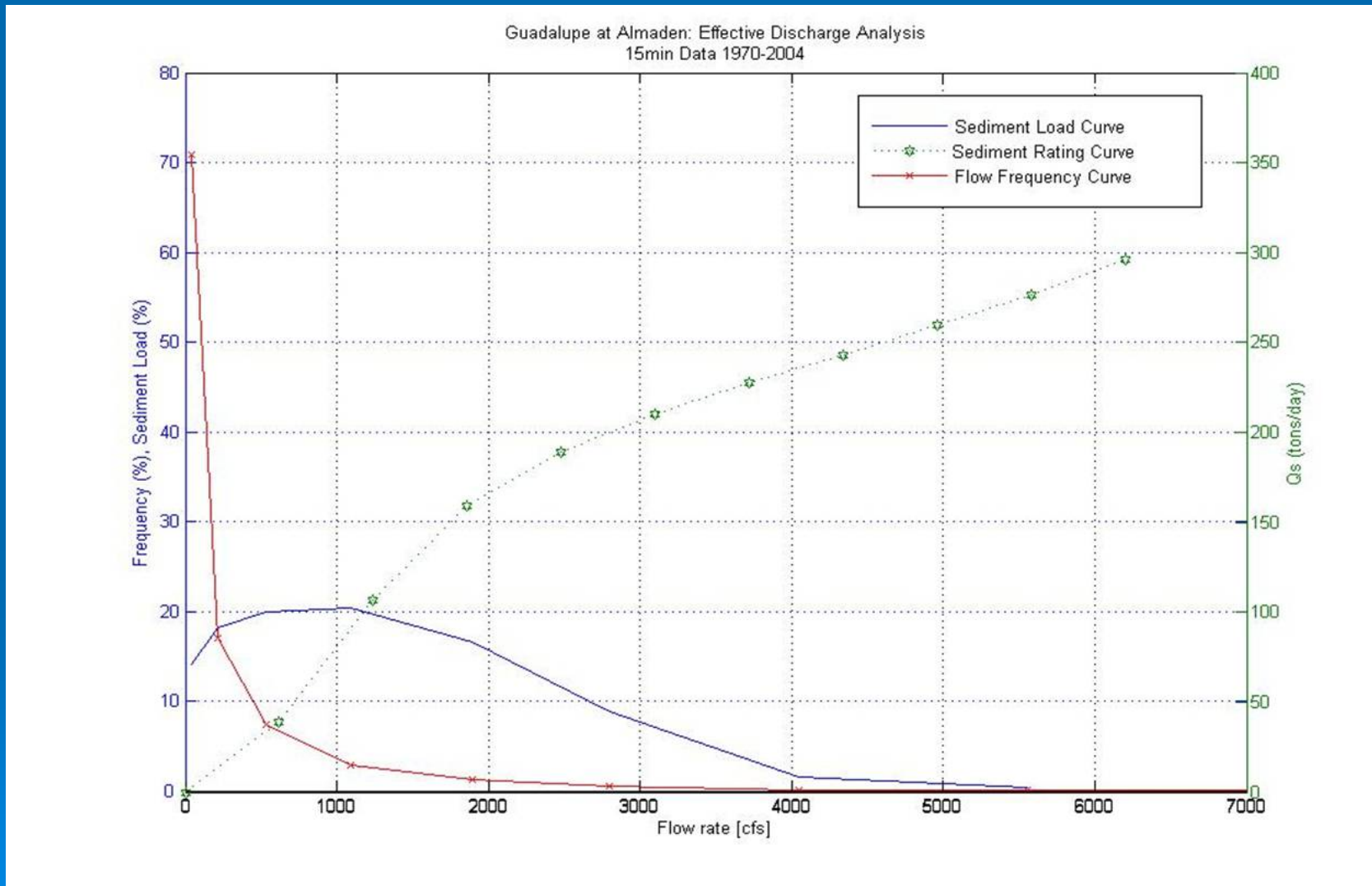
Bottom shear stress $\tau = \gamma RS$

Bankfull Effect on Bottom Shear

**Bottom Shear Stress vs. Flow
For Various Floodplain Widths**



Effective Flow Calculation

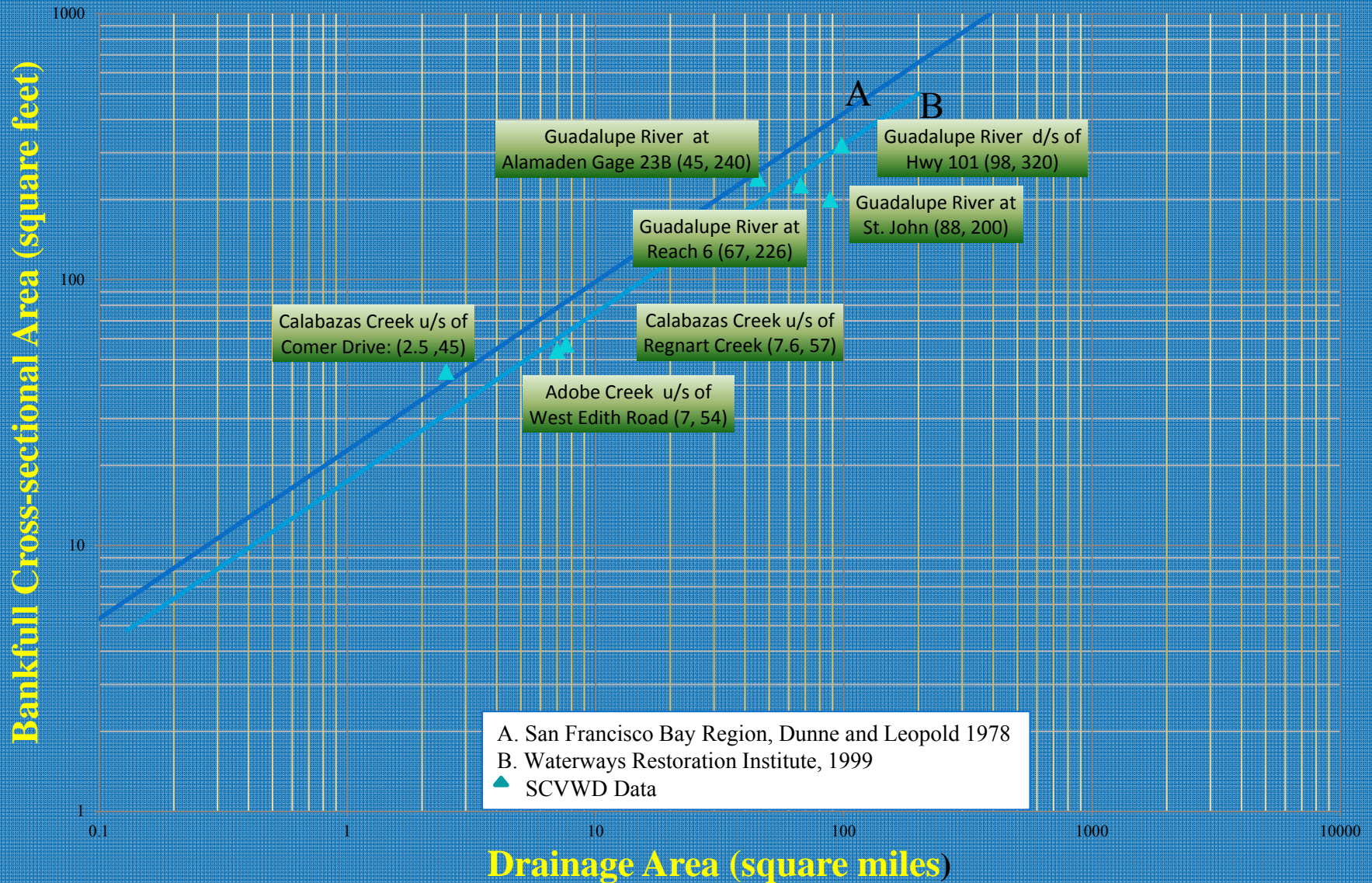


Effective Flow Calculation Results

Gauge Station	Available Gauge Data	Drainage Area (sq mi)	Effective Flow (cfs)	Sediment Transported	Exceedance Frequency (Return Period)
Los Gatos Creek at Lark Ave	1992-2007	6 (44)*	50	45%	94% (1.1)
Ross Creek at Cherry Ave	1956-2007	10	100-200	54%	95-99% (1-1.1)
San Francisquito Creek at Stanford	1987-2007	37	200-500	66%	86-95% (1.1-1.2)
Guadalupe River at Almaden	1970-2004	45 (70)*	700	55%	78-86% (1.2-1.3)
Guadalupe River at Saint John	1987-2003	88 (150)*	900	60%	88% (1.1)
Calabazas Creek at Lawrence	1972-2004	12	250-350	54%	93-97% (1-1.1)
Matadero Creek at Palo Alto	1987-2007	27	270	50%	80% (1.3)

()* denotes drainage area including the areas upstream of the reservoir

Drainage Area vs. Bankfull X-sec



Santa Clara Valley Water District

Bankfull Discharge as a function of Drainage Area



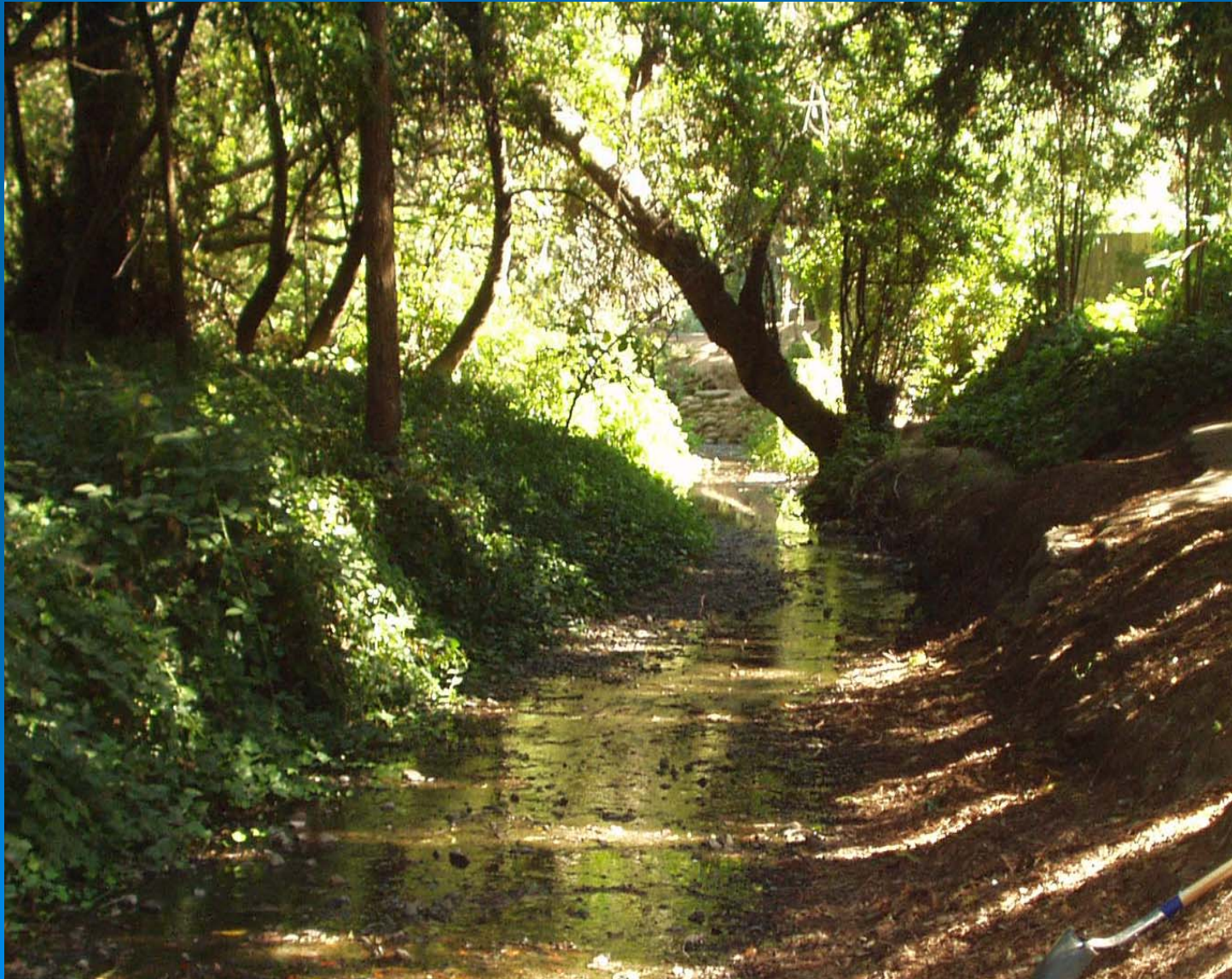
Comer Debris Basin Dam Removal

- Debris basin behind dam has silted in
 - Reduced Passage under Comer Dr. Br.
 - Increased Flooding Potential
- Remove Comer Dam
- Design stable channel

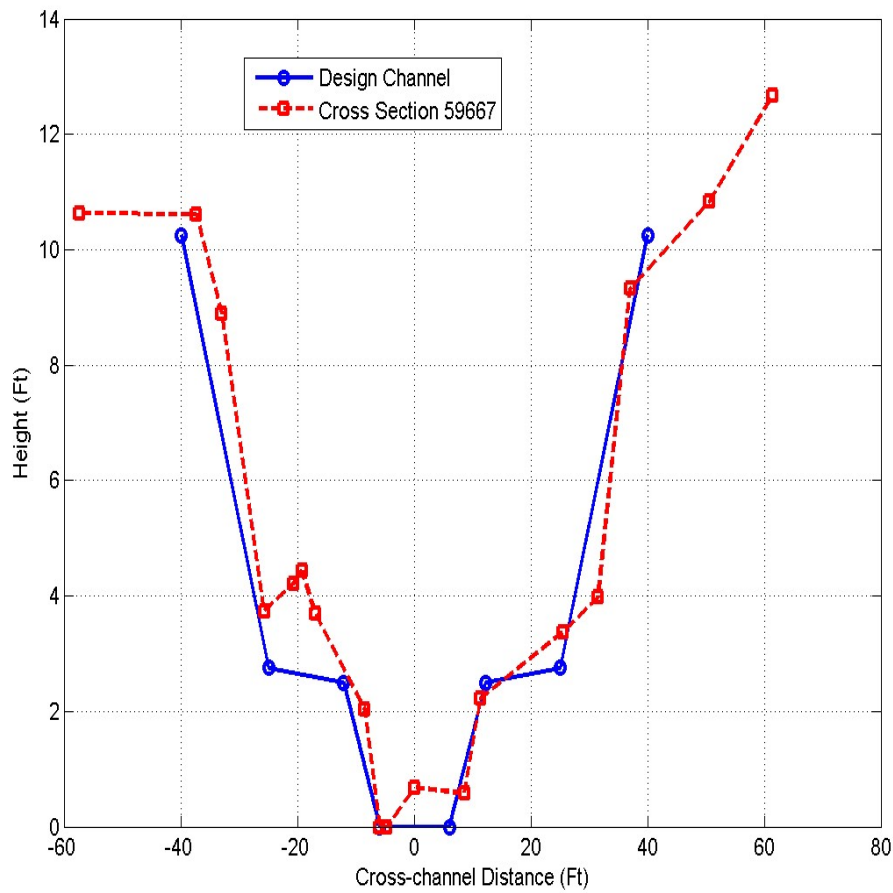
Comer Debris Basin



Reference Reach

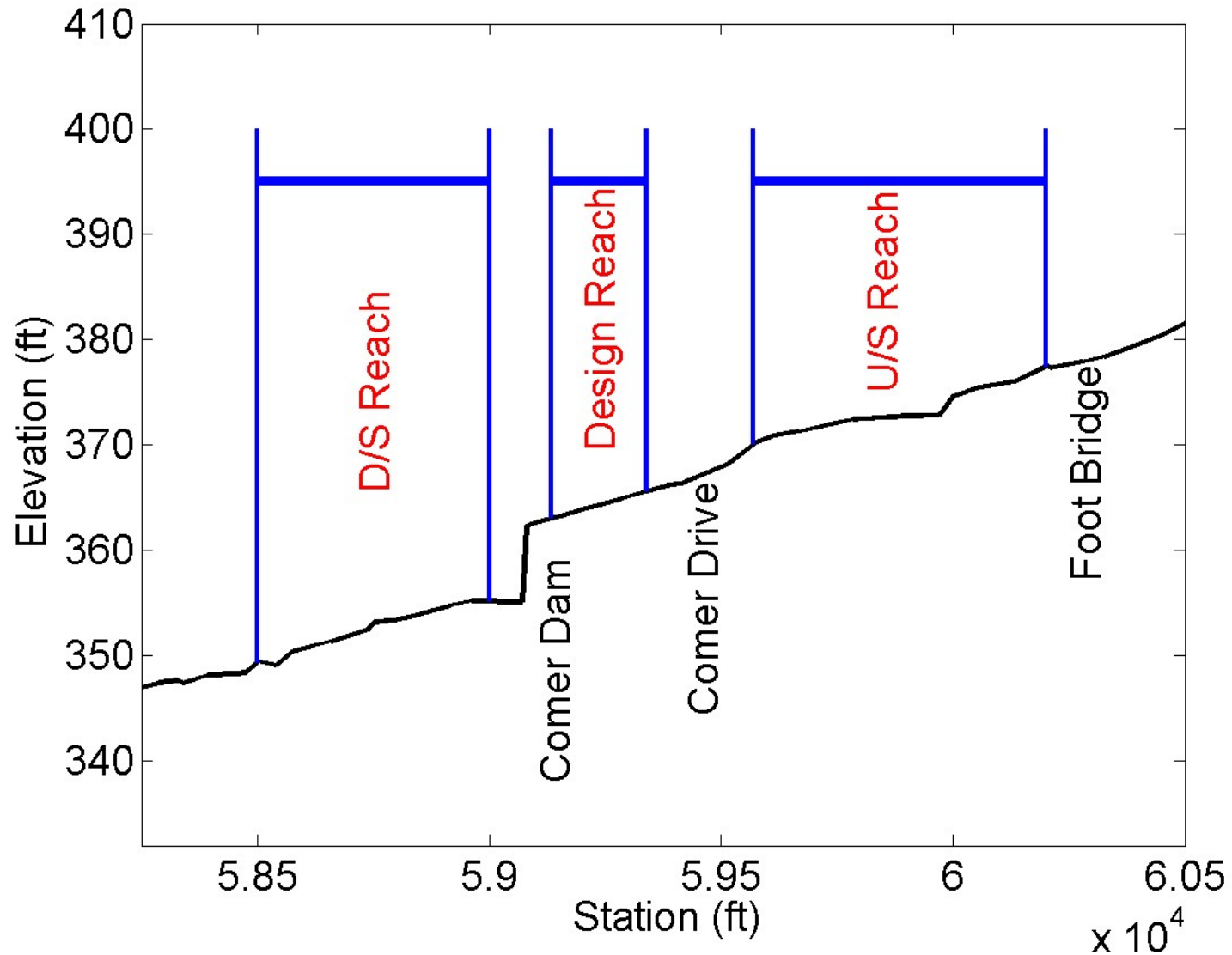


Step 1. Design Stable Cross Section



- Locate stable reach near project area
- Measure bankfull channel dimensions and floodplain slope in field
- Average measurements
- Develop prototypical bankfull channel
- Fit into existing channel by varying floodplain width

Step 2. Estimate Stable Channel Slope



Use SAM to compute Qs: Iteration #1

	Bed Slope (ft/ft)	Qs at bankfull flow (tons/day)
U/S Reach	1.26%	1969
Design Reach	1.25%	3110
D/S Reach	0.9%	2308

Iteration #2

Qs in design reach too large → Reduce slope

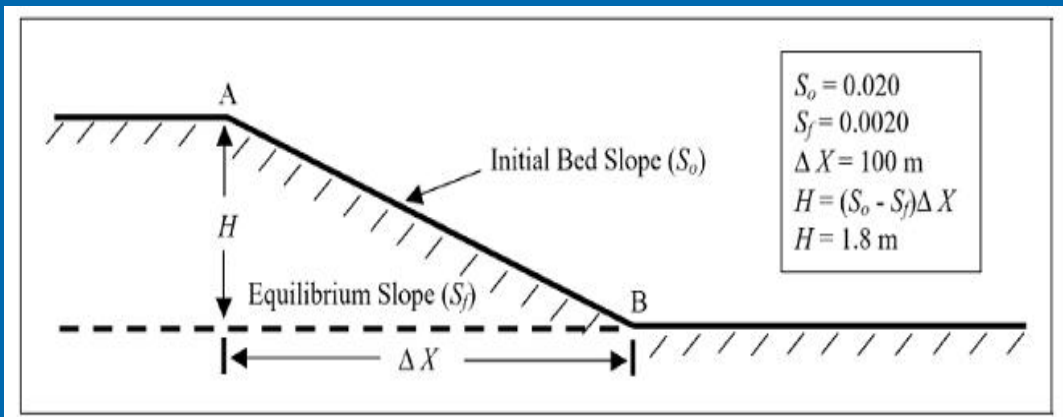
	Bed Slope (ft/ft)	Qs at bankfull flow (tons/day)
U/S Reach	1.26%	1969
Design Reach	1%	2411
D/S Reach	0.9%	2308

Iteration #3: Qs in design reach
between Qs u/s and d/s: DONE !!!

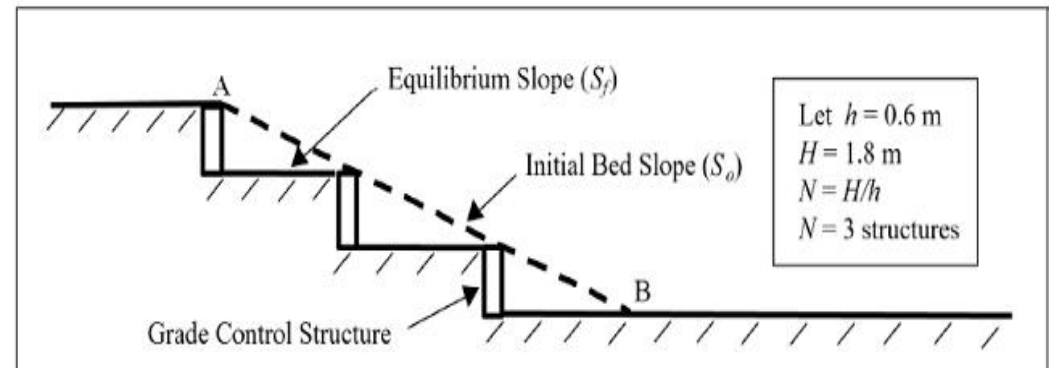
	Bed Slope (ft/ft)	Qs at bankfull flow (tons/day)
U/S Reach	1.26%	1969
Design Reach	0.9%	2103
D/S Reach	0.9%	2308

4. Layout cross-section & profile

- Determine need for grade control
- Design grade control structures (chapter 8, hydraulic design manual)
- Layout plan and profile (workshop in Mar 07)



a. Initial condition of streambed showing degradational zone between points A and B. Total anticipated drop in reach is calculated to be 1.8 m



b. Stabilization of degradational zone using three bed control structures. Each structure has a design drop of 0.6 m

5. Design surface protection

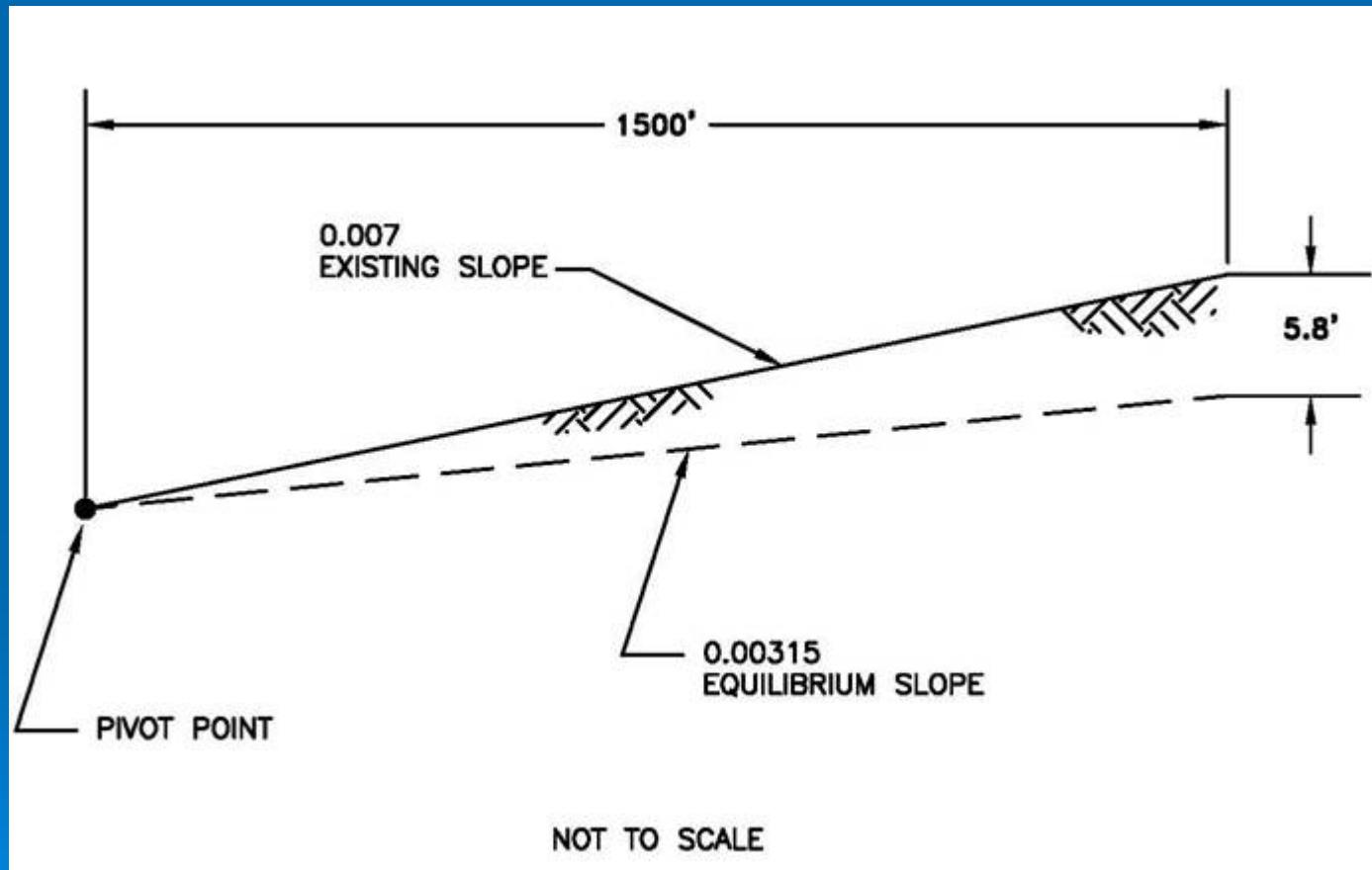
- Although equilibrium slope provides sediment balance, there is continuous sediment deposition and erosion taking place
- Surface armor concept – armor will occur if $D_{\text{critical}} \leq D_{90}$ and the D_{90} materials will cover bed surface
- Surface cover should be compatible with flow regime
- To be described in sediment transport workshop



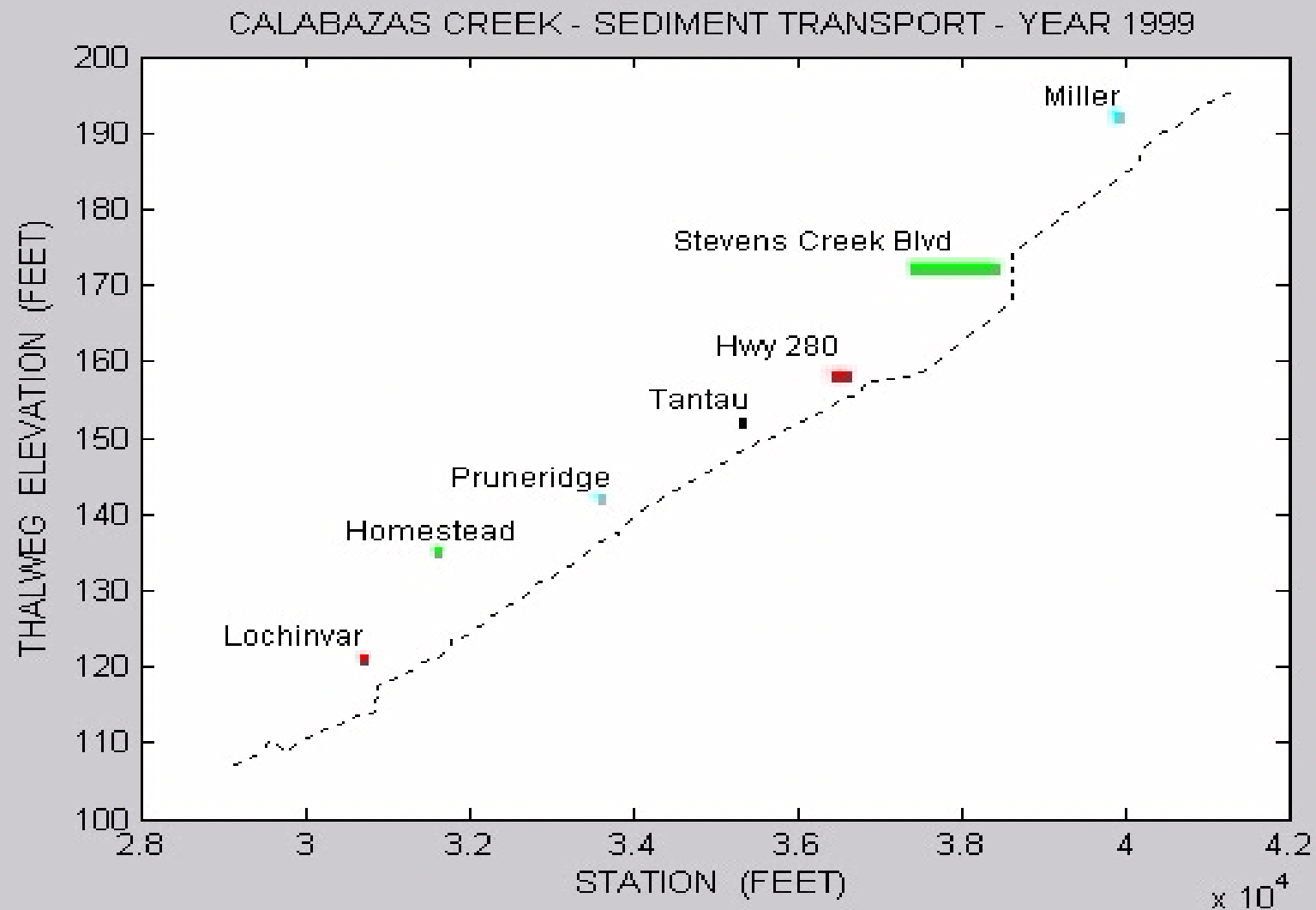
Calabazas Creek Degradation



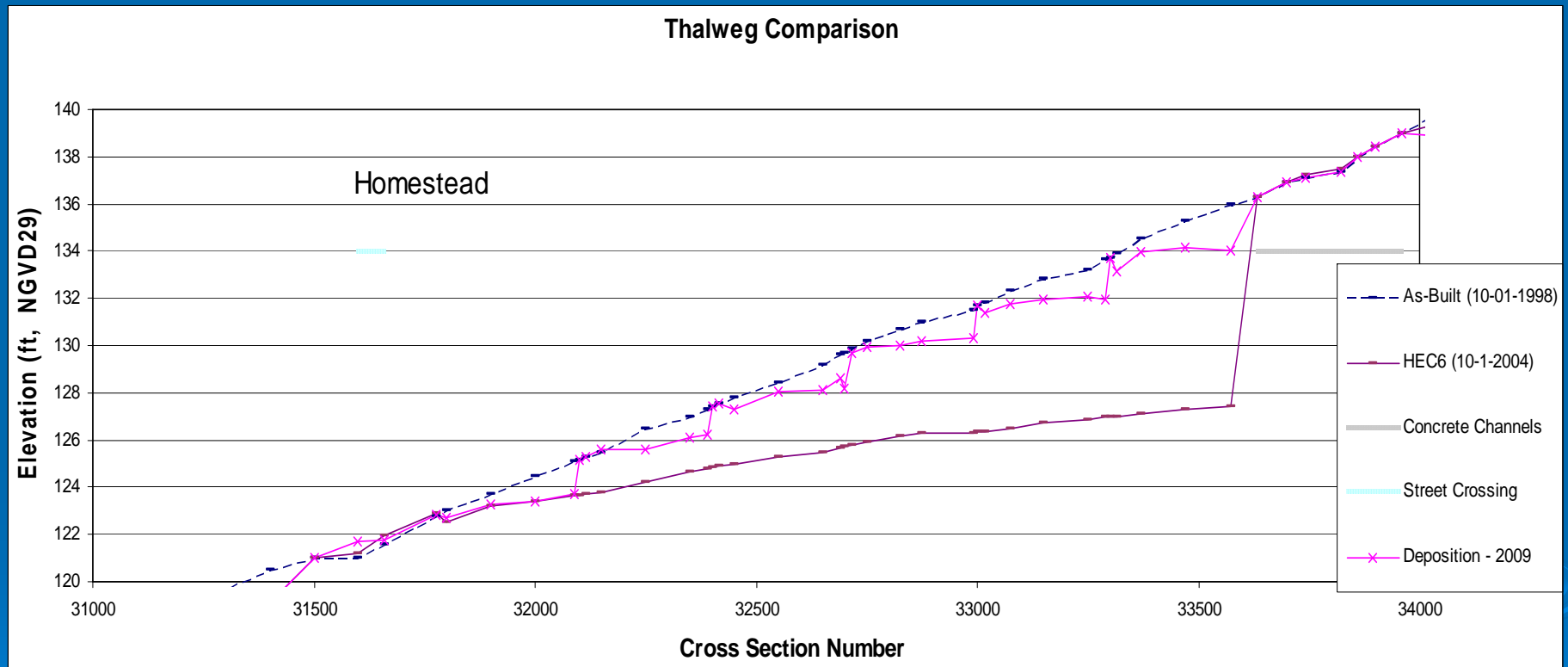
Calabazas Creek Degradation



HEC-6 Sediment Transport Analysis



HEC-6 Results for Post Weir Construction



Weir Construction





11/15/2013

Conclusion

- Understand meaning and origin of geomorphologic parameters
- Focus on applicable parameters and incorporate into design
- SCVWD channel modification designs include field data collection and sediment transport modeling
- Emphasize on long term *stability*

Thanks for Listening!

**DO YOU HAVE ANY
QUESTIONS?**